

### Power- and Spectral-Dependent Photon-Recycling Effects in a **Double-Junction Gallium Arsenide Photodiode**

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Supporting Information

ABSTRACT: Photon-recycling effects improve radiative efficiencies of semiconductor materials and play important roles in the design of high-performance optoelectronic devices. Conventional research mostly studies the impact of photon-recycling on the voltage of photodiodes. Here we systematically analyze the photon response of a microscale gallium-arsenide (GaAs)-based double-junction photodiode. In such a device, the current-matching condition between two



subcells is determined by their photon coupling. Photodynamics in the device is examined and reveals the material's internal quantum efficiencies. By leveraging photon distributions inside the device, we discover that its photocurrent and spectral responses are highly dependent on the illumination intensity. Consistent with theoretical analyses, the device's photocurrents exhibit linear and superlinear power-dependent characteristics under near-infrared and violet-blue illuminations, respectively. Because of the strongly enhanced photon-recycling effects under strong illumination, broadband photon responses (external quantum efficiency close to 50% from 400 to 800 nm) could be achieved in such a strongly current mismatched GaAs dualjunction device. The understanding of photon processes in such devices would offer routes to the design of high-performance photodetectors and solar cells.

KEYWORDS: photon recycling, gallium arsenide, photovoltaics, photodetectors, multijunction

Inderstanding and engineering optical processes in semiconductor materials are critically important to realize high-performance optoelectronic devices such as photovoltaic (PV) cells, photodetectors, light-emitting diodes (LEDs), and lasers.<sup>1,2</sup> In luminescent semiconductors, photon absorption, re-emission, and self-absorption processes, which are also known as the photon-recycling effects, are of tremendous interest in the study of photon receivers. In particular, remarkable results have been recently demonstrated on III-V and halide-perovskite-based semiconductors, in which improved photon-recycling effects lead to a singlejunction or multijunction PV cells with ultrahigh powerconversion efficiencies.<sup>3-7</sup> In these PV cells, enhanced photonrecycling effects increase the open-circuit voltages  $(V_{oc})$ , making cell operation approach the detailed balance limit.<sup>8-11</sup> In general, photon-recycling effects are mostly explored under standard one-sun illumination in PV cells, where various strategies like reflector optimization and lighttrapping design have been implemented to manipulate the internally radiated photons.<sup>12–14</sup> Meanwhile, optoelectronic properties (quantum efficiencies, carrier lifetimes, etc.) of semiconductor materials and devices are dependent on the wavelength and the power of the incident light,<sup>15,16</sup> of which the influences on photon-recycling are, however, less

investigated. In particular, in multijunction devices, the photon processes vary under different current-matching conditions.<sup>7,17</sup> In this Letter, we examine the photon-recycling process in a thin-film microscale gallium-arsenide (GaAs)-based doublejunction photodiode. Photon and carrier-transport behaviors under irradiation at various wavelengths and intensities are experimentally and analytically studied. In such a device, we discover that incident wavelengths affect the current-matching conditions, which lead to varied photon-recycling effects. Under violet-blue (400-480 nm) and near-infrared (near-IR) (~800 nm) illuminations, the output currents exhibit remarkably different dependences on incident powers. These results suggest that photon-recycling effects play a vital role in the optoelectronic device design.

#### RESULTS AND DISCUSSION

Figure 1a schematically illustrates the device layout of a fabricated thin-film GaAs double-junction photodiode used in this study. The epitaxial device structure contains two GaAsbased pn diodes connected with an ultrathin (~22 nm) GaAs-

Received: October 9, 2018 Published: January 2, 2019



Figure 1. (a) Schematic illustration of the GaAs double-junction photodiode. Different colors represent different materials and structures, including p and n contact layers, a top cell, a tunnel junction, and a bottom cell. (b) Bright-field microscopic image of a fabricated GaAs double-junction photodiode (top view). (c) Simulated and (d) measured external quantum efficiency (EQE) spectra of a GaAs double-junction photodiode and its subcells.



**Figure 2.** (a,b) Cartoon illustrations of optical processes (absorption and photon-recycling) inside the GaAs double-junction photodiode under (a) 475 and (b) 810 nm light illumination, respectively. (c) Calculated photon distribution inside the device under 475 nm illumination as a function of depth, considering photon-recycling effects with different internal quantum efficiencies ( $\eta_{int} = 0, 0.1, 1, 10, 50$ , and 100%). (d) Calculated current density–voltage characteristics for the top cell (black dashed line) and the bottom cell (colored lines) with corresponding  $\eta_{int}$  (0.1, 1, 10, and 50%). The intersection points represent the working conditions of subcells in the GaAs double-junction photodiode under the short-circuit condition at 475 nm.



**Figure 3.** (a,b) Time-resolved photoluminescence (TRPL) decay measured for a GaAs double-junction photodiode under femtosecond laser illumination with different power densities at (a) 800 nm (from top to bottom:  $1.4 \times 10^7$ ,  $1.4 \times 10^6$ ,  $7.0 \times 10^5$ ,  $4.2 \times 10^5$ ,  $2.8 \times 10^5$ ,  $1.4 \times 10^5$ , and  $1.4 \times 10^4$  W/m<sup>2</sup>) and (b) 410 nm (from top to bottom:  $1.4 \times 10^7$ ,  $9.2 \times 10^6$ ,  $3.0 \times 10^6$ ,  $1.5 \times 10^6$ ,  $1.2 \times 10^6$ ,  $9.2 \times 10^5$ ,  $3.0 \times 10^5$ ,  $1.5 \times$ 

based tunnel junction. The thicknesses of the top and the bottom GaAs cells are, respectively, designed to be 680 and 1730 nm to realize the current-matching condition and the optimal responsivity at the wavelength of ~800 nm.<sup>18</sup> Instead of using an indium gallium phosphide (InGaP)/GaAs-based double-junction cell conventionally applied for PV research, here we employ a GaAs/GaAs double-junction photodiode structure because: (1) We optimize the device layers to achieve optimal responses around 800 nm as an efficient near-IR photodetector.<sup>18</sup> (2) GaAs is better for studying photonrecycling processes than InGaP because it has higher internal quantum efficiencies.<sup>19</sup> (3) Serially connected ultrathin GaAs junctions demonstrate high output voltages associated with their more efficient carrier collection compared with the thicker counterpart.<sup>7</sup> (4) Such highly current mismatched dual-junction devices show strong power-dependent photonrecycling processes.<sup>17</sup> The microscale device is lithographically defined, metalized, and chemically released from the original growth substrate, forming a thin-film freestanding GaAs double-junction photodiode that can be integrated onto any foreign substrates. Figure 1b illustrates such a GaAs doublejunction photodiode on glass via transfer printing methods,  $^{20-23}$  with lateral dimensions of 700 imes 700  $\mu m^2$  and a thickness of 3.8  $\mu$ m. External quantum efficiency (EQE) spectra of the entire device, the top and the bottom subcells, are calculated based on the finite-element method (Silvaco) and are plotted in Figure 1c. As we designed, the combined device reaches the maximum EQE at ~800 nm, where each subcell absorbs an equivalent amount of photons, and currents are matched between the cells. At other wavelengths, the combined EQE decreases because the device operation deviates from the current-matching condition, and the overall

current is determined by the subcell with a smaller current output. Figure 1d plots the experimental results, in which the EQE spectra of the top and the bottom cells are measured under 850 and 470 nm saturated bias lights, respectively. In this setup, the irradiation intensity of monochromator light is  $1-3 \text{ mW/cm}^2$ . The experimental and calculated results are in a good agreement, with some discrepancies ascribed to the thickness variation during epi-layer deposition as well as the unwanted carrier losses at the surfaces.

The EQE results of the double-junction photodiode are schematically explained in Figure 2a,b. Here we analyze the device response under monochromatic illuminations with 475 nm blue light (Figure 2a) and 810 nm IR light (Figure 2b) and assume that GaAs is nonluminescent under weak irradiation. On the basis of the Beer–Lambert law,<sup>24</sup> we can calculate the absorbed photon distribution across the device thickness. For GaAs, optical absorption lengths at 475 and 810 nm are about 68 and 769 nm, respectively.<sup>25</sup> At 475 nm, most (>99%) photons are captured and absorbed by the top GaAs cell, generating many more free carriers than the bottom cell does (Figure 2a). When the two subcells are connected in series and measured under the short-circuit condition (V = 0), the negligible overall photocurrent is produced, resulting in an EQE close to zero. By contrast, the IR light at 810 nm can penetrate more deeply into the GaAs layers, leading to a more uniform photon distribution (Figure 2b). Therefore, current matching can be realized, and the maximum EQE is achieved.

However, in highly luminescent materials like GaAs, photons and carriers can be "recycled" via re-emission and reabsorption if they cannot be collected by the external circuit due to current mismatch. Such photon-recycling effects could, in turn, alter the photon distribution inside the device.<sup>17,26–28</sup> As



**Figure 4.** (a,b) Current–voltage curves of a GaAs double-junction photodiode measured under varied illumination power densities at (a) 810 (from top to bottom:  $1.4 \times 10^4$ ,  $6.8 \times 10^3$ ,  $4.4 \times 10^3$ ,  $2.4 \times 10^3$ , and  $1 \times 10^{-2}$  W/m<sup>2</sup>) and (b) 475 nm (from top to bottom:  $6.1 \times 10^5$ ,  $5.1 \times 10^5$ ,  $3.5 \times 10^5$ ,  $2.6 \times 10^5$ , and  $1.5 \times 10^5$  W/m<sup>2</sup>), respectively. (c) Measured (scattered dots) and calculated (dashed line) current densities of the GaAs double-junction photodiode as a function of excitation power density at 810 (red) and 475 nm (blue). (d) Conceptual illustrations of the photon-recycling effects on EQE spectra of the double-junction photodiode with different radiative efficiencies (0, 30, 60, and 100%).

illustrated in Figure 2a, photogenerated electrons and holes in the top cell are trapped and undergo recombination via radiative and nonradiative processes. Radiative recombinations create re-emitted photons at the semiconductor band edge (for GaAs, wavelength ~870 nm at room temperature), which redistribute in the entire device, generate photocarriers in both top and bottom cells, and lead to nonzero photocurrent. The varied photon distributions are determined by the radiative efficiencies of GaAs (i.e., internal quantum efficiencies,  $\eta_{int}$ ). Figure 2c plots the calculated photon distribution (including both incident photons at 475 nm and re-emitted photons at 870 nm) as a function of depth in GaAs with different  $\eta_{int}$ based on the Beer–Lambert law (details in the Supporting Information S1).<sup>24</sup> When  $\eta_{int} = 0$ , the illumination is dominated by the 475 nm blue light, with the distribution strictly obeying the Beer-Lambert law. As  $\eta_{int}$  increases, reemitted photons at 870 nm need to be taken into account, which penetrate into the deeper region due to the reduced absorption coefficient in GaAs. Consequently, the bottom cell operation could be significantly influenced by such photonrecycling processes, as shown in Figure 2d. Here we assume that the 475 nm blue illumination has an incident power of 400 W/m<sup>2</sup> and calculate current-voltage characteristics for each cell in the GaAs double-junction photodiode with different  $\eta_{int}$ . When the combined device (overall current, I, and overall voltage, V) is operated under the short-circuit condition (V =0), currents and voltages for the two subcells (top cell:  $I_1$ ,  $V_1$ ; bottom cell:  $I_2$ ,  $V_2$ ) should satisfy

$$I = I_1 = I_2 V_1 + V_2 = 0$$
(1)

The intersection points in Figure 2d represent the working conditions of the subcells for the GaAs double-junction photodiode at 475 nm. Under these scenarios, the top cell is forward-biased and emits IR photons, whereas the bottom cell receives the recycled IR photons and works at the reverse bias. By contrast, such photon-recycling effects are negligible at the incidence of 810 nm (Figure 2b) because the photogenerated carriers are immediately collected by the external circuit under the current-matching condition.

To reveal the photocarrier dynamics of the device, timeresolved photoluminescence (TRPL) measurements are performed under different excitation wavelengths with a femtosecond laser. Figure 3a,b shows the PL decays of a GaAs double-junction photodiode measured at 800 (power density from  $1.4 \times 10^4$  to  $1.4 \times 10^7$  W/m<sup>2</sup>) and 410 nm (power density from  $9.2 \times 10^4$  to  $1.4 \times 10^7$  W/m<sup>2</sup>), respectively. In Figure 3c, the derived PL decay lifetime  $\tau$  is plotted as a function of photon flux at both wavelengths, in comparison with the fitting curve based on the standard ABC model<sup>29</sup>

$$\tau = \frac{1}{A + B(n_0 + \Delta n) + C\Delta n(n_0 + \Delta n)}$$
(2)

where A represents nonradiative recombination and is a function of excess carrier density, B denotes radiative recombination and is assumed to be a constant  $(1.5 \times 10^{-10} \text{ s}^{-1} \text{ cm}^3)$ ,<sup>15,30</sup> and C is associated with the Auger recombination and can be neglected at relatively low carrier densities.<sup>31</sup> Detailed analyses are presented in the Supporting Information S2. The differences between the analytical fitting curve and measured data in Figure 3c stem from complicated non-

radiative recombination mechanisms (surface defects, deep level traps, etc.), which are difficult to model in eq 2. The internal quantum efficiency ( $\eta_{int}$ ) can be expressed as the ratio between the radiative recombination rate ( $U_{rad}$ ) and the nonradiative recombination rate ( $U_{nonrad}$ )

$$\eta_{\rm int} = \frac{U_{\rm rad}}{U_{\rm rad} + U_{\rm nonrad}} = \frac{B[(p_0 + \Delta p)(n_0 + \Delta n) - n_i^2]}{A\Delta n + B[(p_0 + \Delta p)(n_0 + \Delta n) - n_i^2]}$$
(3)

On the basis of the experimental results of  $\tau$ , we can calculate  $\eta_{\text{int}}$  as a function of photon flux. As shown in Figure 3d,  $\eta_{\text{int}}$  monotonically increases with the absorbed photon flux, which is attributed to the gradual saturation of nonradiative recombination centers.

We further measure the current-voltage characteristics of the GaAs double-junction photodiode under varied illumination power densities at 810 (from 0.02 to  $2.2 \times 10^6 \text{ W/m}^2$ ) and 475 nm (from 300 to  $10^6$  W/m<sup>2</sup>), with results, respectively, illustrated in Figure 4a,b. The device exhibits open-circuit voltages of ~2.0 V, and its photocurrent increases in accordance with the illumination power. The measured current density is plotted in Figure 4c as a function of the excitation power for both 810 (red dots) and 475 nm (blue dots) illuminations. At 810 nm, absorbed photons are nearly equally distributed in each subcell of the GaAs double-junction photodiode. As shown in Figure 1c, calculated photon absorption in both the top cell and the bottom cell is  $\sim 40\%$ . Therefore, the device reaches the current-matching condition, and the output current is linearly proportional to the excitation power (red dashed line)

$$I = I_{\rm nh} \times EQE \; (\lambda = 810 \; \rm nm) \tag{4}$$

where  $I_{\rm ph}$  is the incident photon flux and EQE is ~40%, as calculated and measured in Figure 1.

By contrast, most of the photons at 475 nm are absorbed by the top cell, and only part of photogenerated carriers produce re-emitted photons that can be recycled by the bottom cell, as explained in Figure 2a. Consequently, the overall current is determined by the cell with a smaller current output, which is the bottom cell in this case (details in the Supporting Information S3). Therefore, the output current is dependent on the photon-recycling efficiency

$$I = \frac{I_{\rm ph}}{1 + \frac{1}{\eta_{\rm LC}}} \tag{5}$$

where  $\eta_{LC}$  is defined as the luminescence coupling efficiency and mainly related to  $\eta_{int}$  as well as the device geometry<sup>11</sup>

$$\eta_{\rm LC} = \frac{\eta_{\rm int} P_{\rm LC}}{1 - \eta_{\rm int} \overline{P_{\rm abs}}} \tag{6}$$

where  $\overline{P_{abs}}$  and  $\overline{P_{LC}}$  are the probabilities of internal photons to be reabsorbed inside the top cell itself and to be coupled to the bottom cell in the GaAs double-junction photodiode, both of which are determined by the cell structures (details in the Supporting Information S4). We can get

$$I = \frac{I_{\rm ph}}{1 + \frac{1 - 0.573\eta_{\rm int}}{0.356\eta_{\rm int}}}$$
(7)

By applying the experimentally obtained  $\eta_{int}$  values (Figure 3d) to the above equations, the output current (I) of the GaAs double-junction photodiode can be calculated and plotted in Figure 4c (blue dashed line). The calculation results are consistent with the experiments and exhibit a superlinear relationship with the excitation power density. The remaining discrepancy between experiment and calculated results indicates the existence of additional nonradiative recombination mechanisms in the actual device. Under weak illumination, the photoresponse at 475 nm is orders of magnitude lower than that at 810 nm, in agreement with the measured EQE results in Figure 1d. When the illumination power increases, the photocurrent at 475 nm grows faster than that at 810 nm due to the enhanced photon-recycling effect. Although two monochromatic light sources are used to study the device operation, photon and carrier processes at other wavelengths can be analyzed based on similar principles, depending on the current-match/mismatch states. For such a double-junction device, these results imply that the EQE spectra vary with the illumination intensity at different wavelengths. Figure 4d conceptually predicts such effects based on our observations. Ideally, the EQE spectrum could present a plateau in a wide range when  $\eta_{\rm int}$  approaches 100%, behaving similarly to a single-junction GaAs photodiode but with a doubled output voltage. In this scenario, most free carriers can radiatively recombine and form IR photons that can be recycled by the bottom cell. Therefore, current can be matched between the subcells at most wavelengths. It should be noted that the photon-recycling effect can be diminished at ultrahigh illumination power densities (e.g., for GaAs, >1000 suns) because Auger processes start to dominate the nonradiative recombination.3

#### CONCLUSIONS

To summarize, we investigate the optoelectronic performance of a thin-film GaAs-based double-junction photodiode structure and discover that its photoresponse reveals strong illumination and wavelength dependences associated with the photon-recycling effect. It is well known that the photonrecycling effect plays important roles in the  $V_{oc}$  and efficiency of single-junction devices. Here we demonstrate that the photon-recycling effect also significantly influences the photocurrent in multijunction devices by altering the photon coupling between the subcells. For PV cells and detectors made of highly luminescent materials like GaAs, these results imply that the measured EQE spectra are influenced by the illumination intensity, and broadband photoresponses (EQE close to 50% from 400 to 800 nm) can be realized under highpower irradiation, even by using highly current mismatched multijunction devices. Considering the photon coupling, optimal device structures are power-dependent (for example, for devices under one-sun illumination vs concentrated sunlight). Besides the material quality, other factors such as electrical fields and optical interfaces are also critical and impact the photon recycling. Similar effects can be explored in devices based on other light emitters including III-Vs, halide perovskites, quantum dots, and so on. We anticipate that the results presented here could provide constructive insights into the design of high-performance photodetectors, PV cells, and optical sensors in general.

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#### METHODS AND MATERIALS

Device Fabrication. The GaAs double-junction photodiode structure is grown on a GaAs substrate by using the metal-organic chemical vapor deposition (MOCVD) method. The detailed structure (from top to bottom) consist of an ntype (Si doping,  $6 \times 10^{18}$  cm<sup>-3</sup>) GaAs contact layer (200 nm), a top cell (30/100/450/100 nm, n-type InGaP window (Si doping,  $2 \times 10^{18}$  cm<sup>-3</sup>)/n-type GaAs emitter (Si doping,  $2 \times$  $10^{18}$  cm<sup>-3</sup>)/p-type GaAs base (Zn doping,  $10^{17}$  cm<sup>-3</sup>)/p-type Al<sub>0.3</sub>Ga<sub>0.7</sub>As BSF (Mg doping, 5 ×  $10^{18}$  cm<sup>-3</sup>)), a highly doped tunnel junction layer (p-type (C doping,  $8 \times 10^{19} \text{ cm}^{-3})/n$ type (Se doping,  $9 \times 10^{19}$  cm<sup>-3</sup>) GaAs, 11/11 nm), a bottom cell (30/100/1500/100 nm, n-type Al<sub>0.3</sub>Ga<sub>0.7</sub>As window (Si doping,  $2 \times 10^{18}$  cm<sup>-3</sup>)/n-type GaAs emitter (Si doping,  $2 \times$  $10^{18} \text{ cm}^{-3})/\text{p-type}$  GaAs base (Zn doping,  $10^{17} \text{ cm}^{-3})/\text{p-type}$ InGaP BSF (Mg doping, 10<sup>18</sup> cm<sup>-3</sup>)), a p-type GaAs contact layer (Mg doping,  $5 \times 10^{18}$  cm<sup>-3</sup>, 1000 nm), a sacrificial layer (Al<sub>0.95</sub>Ga<sub>0.05</sub>As, 500 nm), and the GaAs substrate. All of the layers are lattice-matched to the GaAs substrate. The device is lithographically patterned, and Ge/Ni/Au and Cr/Au serve as ohmic electrodes for n-type and p-type GaAs contact layers, respectively. Freestanding thin-film devices are formed by removing the Al<sub>0.95</sub>Ga<sub>0.05</sub>As sacrificial layer in diluted hydrofluoric-acid (HF)-based solution (HF/water 1:10 by volume, with few drops of ethanol). Using patterned poly-(dimethylsiloxane) (PDMS) stamps, released devices are picked up and transferred to various carrier substrates (glass, polyimide film, silicon, etc.) with a spin-coated adhesive laver.<sup>20</sup>

**Device Characterization.** Current–voltage characteristics are recorded using a Keithley 2400 source meter. Illuminations are provided with various light sources, including a 475 nm diode laser (Changchun New Industries Optoelectronics) and an 810 nm diode laser (Hi-Tech Optoelectronics). EQE spectra are measured using an incident photo-to-charge carrier efficiency (IPCE) measurement system (QEX10, PV Measurement, USA) from 400 to 1000 nm, of which the irradiation intensity of monochromator light is 1–3 mW/cm<sup>2</sup>. The EQE spectra of the top and bottom subcells are measured with the 850 and 470 nm saturated bias lights (light sources: M850L3-C1 and M470L3-C1 from Thorlabs), respectively.

TRPL measurements are taken using an ultrafast pulse laser from a Spectra-Physics Mai Tai apparatus (410 or 800 nm, 80 MHz, ~120 fs). The laser spot sizes are ~80  $\mu$ m. The emission light passes through an 830 nm long pass filter (BLP01-830R-25, Semrock) and is collected by a single-photon avalanche photodiode detector (TDA 200) combined with a timecorrelated single photon-counting module (TimeHarp 260 PICO Single).

#### ASSOCIATED CONTENT

#### **S** Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsphotonics.8b01404.

Detailed analytical calculation for short-circuit current  $(I_{sc})$  of GaAs double-junction photodiode by considering the photon-recycling effects (PDF)

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#### Notes

The authors declare no competing financial interest.

#### ACKNOWLEDGMENTS

This work is supported by the National Natural Science Foundation of China (grants 51602172 and 61874064). X.S. also acknowledges support from the Beijing Innovation Center for Future Chips, Tsinghua University.

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## Supporting Information for

# Power- and Spectral-Dependent Photon-Recycling Effects in a Double-Junction Gallium Arsenide Photodiode

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#### **Contents:**

- S1. Photon distribution
- S2. Carrier Recombination

S3. Luminescence coupling efficiency of the GaAs double junction photodiode

S4. Short-circuit current of the GaAs double junction photodiode

We analytically calculate the relationship between short-circuit current ( $I_{sc}$ ) of GaAs double junction photodiode and excitation power density (P), considering the photon-recycling effects.

### **S1.** Photon Distribution

The photon distribution is calculated based on a phenomenological approach using the absorption coefficient ( $\alpha$ ) of GaAs at 475 nm (excitation wavelength,  $\alpha = 1.511 \times 10^7 \text{ m}^{-1}$ ) and 870 nm (band edge of GaAs,  $\alpha = 8 \times 10^5 \text{ m}^{-1}$ ).<sup>1</sup> A semi-infinitely large semiconductor bulk (thickness: *z* from 0 to  $\infty$ ) is assumed, and we calculate the number of photons both at wavelength of 475 nm ( $N_{475}$ ) and 870 nm ( $N_{870}$ ) as a function of the thickness.

The photons at a wavelength of 475 nm derive from the external irradiation light, which is conformed to the Beer–Lambert Law<sup>2</sup>:

$$N_{475}(z) = N_{475}^0 \exp(-\alpha_{475} z) \tag{1}$$

The photons at a wavelength of 475 nm derive from the photon-recycling effect, which is initially generated by the photons at a wavelength of 475 nm and related to the internal quantum efficiency ( $\eta_{int}$ ) of the material.

$$dN_{870}(z) = -\eta_{int} dN_{475}(z) - \alpha_{870} N_{870}(z) dz$$

$$N_{870}(z) = N_{475}^0 \frac{\alpha_{475}}{\alpha_{475} - \alpha_{870}} \eta_{int} \left( \exp(-\alpha_{870} z) - \exp(-\alpha_{475} z) \right)$$
(2)

And the total photon distribution is sum of the  $N_{475}$  and  $N_{870}$ :

$$N(z) = N_{475}(z) + N_{870}(z)$$

$$= \frac{\alpha_{475}}{\alpha_{475} - \alpha_{870}} N_{475}^0 \left( \eta_{\text{int}} \exp(-\alpha_{870} z) + \left(1 - \eta_{\text{int}} - \frac{\alpha_{870}}{\alpha_{475}}\right) \exp(-\alpha_{475} z) \right)$$
(3)

Furthermore, as the tremendous differences of  $\alpha$  between the wavelength of 870 nm and 475 nm ( $\alpha_{870} / \alpha_{475} \approx 0$ ), the photon distribution can be further simplified as:

$$N(z) = N_{475}^0 \left( \eta_{\text{int}} \exp(-\alpha_{870} z) + (1 - \eta_{\text{int}}) \exp(-\alpha_{475} z) \right)$$
(4)

which is a linear combination of the Beer–Lambert law for the wavelength of 870 nm and 475 nm.

## **S2.** Carrier Recombination

In the ABC model, the carrier recombination rate (R) in a bulk semiconductor material is expressed with the carrier density (n):

$$R = An + Bn^2 + Cn^3 \tag{5}$$

In this model, the SRH recombination is represented by coefficient *A* (or its reciprocal, nonradiative carrier lifetime,  $\tau_{nr}$ ).<sup>3–5</sup> Thus,  $\tau_{nr}$  can be expressed as:

$$\tau_{\rm nr} = \frac{1}{A} = \left(\tau_{\rm p0} \frac{n_0 + n_1}{n_0 + p_0} + \tau_{\rm n0} \frac{p_0 + p_1}{n_0 + p_0}\right) \frac{1 + \frac{\Delta n \left(\tau_{\rm p0} + \tau_{\rm n0}\right)}{\tau_{\rm p0} \left(n_0 + n_1\right) + \tau_{\rm n0} \left(p_0 + p_1\right)}}{1 + \frac{\Delta n}{n_0 + p_0}} \tag{6}$$

where  $n_0$  and  $p_0$  are electron and hole equilibrium density,  $\Delta n$  is excess carrier density,  $\tau_{p0}$ and  $\tau_{n0}$  are two lifetime constants (unrelated to carrier density),  $n_1$  and  $p_1$  are defined as following if  $E_t$  is the trap energy level:

$$n_{1} = N_{C} \exp\left(-\frac{E_{C} - E_{t}}{kT}\right)$$

$$p_{1} = N_{V} \exp\left(-\frac{E_{t} - E_{V}}{kT}\right)$$
(7)

In general,  $n_0$  is relatively large and  $p_0$  is very small in an n-type semiconductor.<sup>3</sup> If the trap energy level  $E_t$  is in the middle of the bandgap,  $n_1$  and  $p_1$  can also be negligible. Therefore, the formula above can be simplified to

$$\tau_{\rm nr} = \frac{1}{A} = \frac{\tau_{\rm p0} + \frac{\Delta n}{n_0} (\tau_{\rm p0} + \tau_{\rm n0})}{1 + \frac{\Delta n}{n_0}}$$
(8)

When  $\Delta n$  is zero,  $\tau_{nr} = \tau_{p0}$ , which equals to the minority carrier nonradiative lifetime. When  $\Delta n$  approaches infinity,  $\tau_{nr} = \tau_{p0} + \tau_{n0}$ , which is the sum of the majority and the minority carrier nonradiative lifetime. In general, as  $\Delta n$  is monotonously dependent on  $\tau_{nr}$ , the coefficient *A* gets smaller at higher excitation levels.

And the radiative recombination process is represented by coefficient *B* in this model, which is mainly determined by temperature (*T*) and the absorption coefficient ( $\alpha$ ):

$$B = \frac{8\pi}{h^3 c_0^2 n_i^2} \int_0^\infty n^2 \left(h\nu\right)^2 \alpha \left(h\nu, T\right) \exp\left(-\frac{h\nu}{kT}\right) d\left(h\nu\right)$$
(9)

For GaAs at the temperature of 300 K, the coefficient *B* is assumed to be independent of carrier density *n*, and is set to be a constant  $1.5 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>.<sup>5, 6</sup>

The Auger recombination process, which is represented by coefficient C, consists of the conduction-band Auger process (CHCC) and the valence-band Auger process (CHSH). For CHCC, the Auger coefficient is determined by the related band structure (and vice versa for CHSH), and can be expressed as:

$$C = \frac{4\pi^{1/2}h^2g(E)e^4F}{(2m_vkT)^{3/2}} \frac{k_0^2}{E_c(k_0) - E_v(k_0)} \exp\left(-\frac{E_v(k_0)}{kT}\right)$$
(10)

where g(E) is the state density function, and  $k_0$  is the wave vector in the conduction band.<sup>7</sup> In most scenarios, the Auger recombination coefficient (*C*) of GaAs is normally smaller than  $10^{-30}$  cm<sup>6</sup> s<sup>-1</sup>, so the influence of Auger recombination can be neglected if the carrier density is lower than  $10^{20}$  cm<sup>-3</sup>.<sup>8-11</sup> Thus, the coefficient *C* is negligible in this analysis due to the low excitation power density ( $P < 1.4 \times 10^7$  W/m<sup>2</sup>) and the corresponding low carrier density ( $n < 10^{18}$  cm<sup>-3</sup>).

# S3. Luminescence coupling efficiency of the GaAs double junction photodiode

Under steady state condition, the carrier generation rate and the total recombination rate should be equal. Assuming a uniform distribution of carriers in the top cell, the excess carrier density is determined by the excitation power density:

$$A\Delta n + B\Big[\Big(p_0 + \Delta p\Big)\Big(n_0 + \Delta n\Big) - n_i^2\Big] = \frac{P}{h\nu L_1}$$
(11)

where  $\Delta n = \Delta p$  is the excess carrier density,  $p_0$  and  $n_0$  are equilibrium carrier densities,  $n_i$  is the intrinsic carrier density, P is the incident power density, v is the frequency of incident light, and  $L_1$  is the thickness of the top cell (cell 1). As IQE ( $\eta_{int}$ ) is the ratio of the radiative recombination rate and the total recombination rate,  $\eta_{int}$  can be expressed as a function of excitation power density:

$$\eta_{\text{int}}(P) = \frac{U_{\text{rad}}}{U_{\text{rad}} + U_{\text{nonrad}}} = \frac{B\left[\left(p_0 + \Delta p(P)\right)\left(n_0 + \Delta n(P)\right) - n_i^2\right]}{A\Delta n(P) + B\left[\left(p_0 + \Delta p(P)\right)\left(n_0 + \Delta n(P)\right) - n_i^2\right]}$$
(12)

Furthermore, by taking reference of the model in Ref.[12], the luminescence coupling efficiency ( $\eta_{LC}$ ) in the GaAs double junction photodiode can be written as:

$$\eta_{\rm LC}(P) = \frac{\eta_{\rm int}(P)P_{\rm LC}}{1 - \eta_{\rm int}(P)\overline{P_{\rm abs}}}$$
(13)

where  $\overline{P_{abs}}$  and  $\overline{P_{LC}}$  are the probabilities of internal photons to be reabsorbed inside the top cell itself and to be coupled to the bottom cell in the GaAs double junction photodiode. They are determined by the optical properties of the GaAs double junction photodiode and the substrate index:

$$\overline{P_{abs}} = 1 - \int_{0}^{\frac{\pi}{2}} \frac{1 - \exp\left(-\frac{\alpha L_{1}}{\cos\theta}\right)}{\alpha L_{1}} \left(1 - \frac{R_{f}\left(\theta\right)}{2} \left(1 - \exp\left(-\frac{\alpha L_{1}}{\cos\theta}\right)\right)\right) \cos\theta\sin\theta\,d\theta$$

$$\overline{P_{LC}} = \int_{0}^{\frac{\pi}{2}} \frac{T_{b}'(\theta) \exp\left(-\frac{\alpha L_{1}}{\cos\theta}\right)}{2\alpha L_{1}} \left(1 + R_{f}\left(\theta\right) \exp\left(-\frac{\alpha L_{1}}{\cos\theta}\right)\right) \sin\theta\cos\theta\,d\theta$$
(14)

where  $\alpha$  is the absorption coefficient of GaAs at its bandgap (870 nm, 8×10<sup>5</sup> m<sup>-1</sup>),  $R_{\rm f}(\theta)$ is the coefficient of reflection that occurs at the top cell-air interface (equals 1 when  $\theta < \sin^{-1}(1/n_{\rm GaAs})$  and otherwise 0) and  $T_{\rm b}(\theta)$  is the coefficient of transmission that occurs at the interface between two subcells, without counting the absorption in the substrate.<sup>12</sup> So, it can be numerically calculated that  $\overline{P_{\rm abs}}$  and  $\overline{P_{\rm LC}}$  of the GaAs double junction photodiode are 57.3% and 35.6%, respectively.

# S4. Short-circuit current of the GaAs double junction photodiode

Based on the detailed balance (DB) theory,<sup>13, 14</sup> the current of the diode is equal to the difference between generated carriers and recombined carriers:

$$I = I_{\text{generation}} - I_{\text{recombination}} = I_{\text{ph}} + I_{\text{th}} - I_{\text{rad}} - I_{\text{nrad}}$$
(15)

where the  $J_{ph}$  is the photogenerated current and derived from the incident photons ( $I_{inc}$ ),  $I_{th}$  is the absorbed thermal radiation from the environment, and the  $I_{rad}$  is the radiative current, and  $I_{nrad}$ is the nonradiative current, and these currents in the device (surface area: *S*) can be expressed in the following equations:

$$I_{\rm ph} = \eta_{\rm abs} I_{\rm inc}$$
(16)  
$$I_{\rm th} = \frac{2\pi \left(n^2 + 1\right) q k T S}{h^3 c^2} E_{\rm g}^2 \exp\left(-\frac{E_{\rm g}}{kT}\right)$$
(17)

$$I_{\rm rad} = \frac{2\pi \left(n^2 + 1\right) q k T S}{h^3 c^2} E_{\rm g}^2 \exp\left(\frac{q V - E_{\rm g}}{kT}\right)$$
(18)  
$$I_{\rm rad} = I_{\rm th} \exp\left(\frac{q V}{kT}\right)$$
(19)

As the external radiative efficiency ( $\eta_{ext}$ ) is defined as:

$$\eta_{\rm ext} = \frac{I_{\rm rad}}{I_{\rm rad} + I_{\rm nrad}} \tag{20}$$

The output current can be shorted to:

$$I = I_{ph} + I_{th} - I_{rad} - I_{nrad}$$
  
=  $I_{ph} + I_{th} - I_{rad} / \eta_{ext}$  (21)  
=  $I_{ph} + I_{th} - I_{th} \exp\left(\frac{qV}{kT}\right) / \eta_{ext}$ 

For the GaAs double junction photodiode irradiated under blue light (475 nm), only the top cell (cell 1,  $I_1$ ,  $V_1$ ) is able to receive the incident light and generate the photocarriers, so the

$$I_1 = I_{\rm ph} + I_{\rm th} - I_{\rm th} \exp\left(\frac{qV_1}{kT}\right) / \eta_{\rm ext}$$
(22)

Similarly, considering the bottom cell (cell 2,  $I_2$ ,  $V_2$ ) can only receive those photons regenerated by electron-hole radiative recombination in the top cell (photon-recycling effect), the current of the bottom cell can be expressed as:

$$I_{2} = I_{\text{ph}_{1} \to 2} + I_{\text{th}} - I_{\text{th}} \exp\left(\frac{qV_{2}}{kT}\right) / \eta_{\text{ext}}$$
(23)

Here, the  $I_{ph_1 \rightarrow 2}$  is the photocurrent generated by the irradiation based on the photon-recycling effect from the top layer, and is determined by  $\eta_{LC}$ :

$$I_{\text{ph}_{1}\rightarrow2} = \left(\eta_{\text{LC}}/\eta_{\text{ext}}\right)I_{1_{\text{rad}}} = \left(\eta_{\text{LC}}/\eta_{\text{ext}}\right)I_{\text{th}}\exp\left(\frac{qV_{1}}{kT}\right)$$
(24)

By taking into account the series connection restrictions, the current and voltage of the subcells can be expressed as:

$$I = I_1 = I_2 V_1 + V_2 = 0$$
(25)

Furthermore, the thermal current  $I_{th}$  is negligible compared to  $J_{ph}$ . So, the short-circuit current ( $I_{sc}$ ) of the GaAs double junction photodiode can be simplified as:

$$I_{\rm sc}(P) = \frac{I_{\rm ph}(P)}{1 + \frac{1}{\eta_{\rm LC}(P)}}$$
(26)

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